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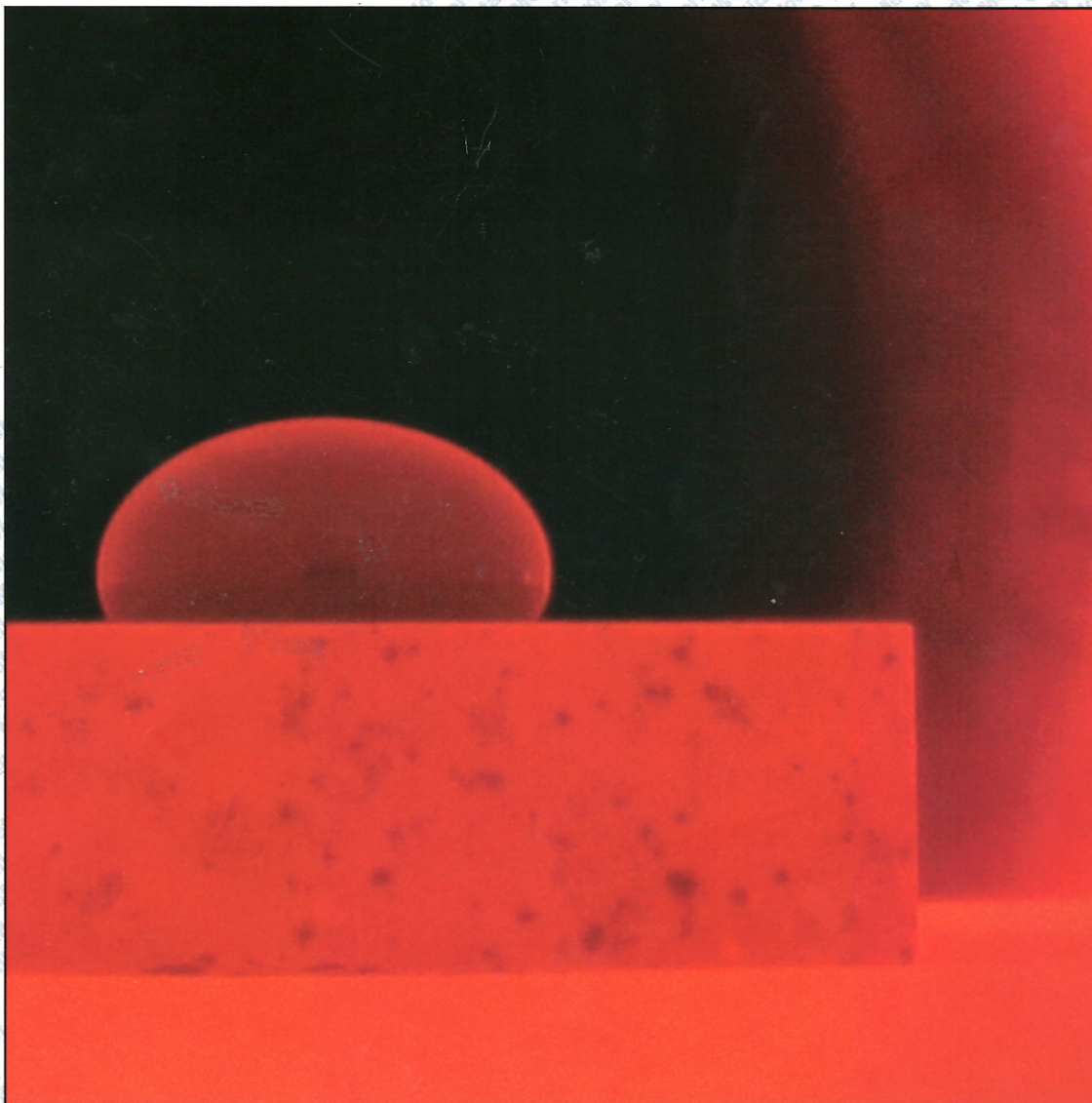
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# Zinc Waste Treatment Originated During Hot-Dip Galvanizing

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The present paper is focused on the research of the hard zinc and top dross treatment possibilities. Hard zinc or bottom dross originates during the hot-dip galvanizing process in the zinc bath and top dross is produced in the continuous process. In this paper wastes are characterized and the attention is paid to chosen kinds of solid wastes. Hard zinc contains 91 to 96 % of zinc. Iron represents an impurity with content of 1 to 6 %. Top dross contains about

1 % Fe and Al and the rest represents zinc. In every case the iron is an unwanted element in drosses. Therefore, the possibilities of hard zinc and top dross treatment with the aim of iron removal are studied in this work.

Keywords:

Hot-dip galvanizing – Waste – Drosses – Iron – Recycling

## Behandlung von zinkhaltigen Rückständen der Tauchfeuerverzinkung

Diese Arbeit untersucht die Möglichkeiten der Behandlung von Hartzink und Oberflächenkrätze. Hartzink oder Bodenkrätze entsteht bei der Tauchfeuerverzinkung, Oberflächenkrätze bei der kontinuierlichen Bandfeuerverzinkung. Rückstände werden charakterisiert und ausgewählte Arten fester Rückstände werden untersucht. Hartzink enthält 91 bis 96 % Zink und als Verunreinigung Eisen mit einem Gehalt von 1 bis 6 %. Oberflächenkrätze enthält ungefähr 1 % Eisen und Aluminium, der Rest besteht aus Zink. In

allen Fällen stellt Eisen ein unerwünschtes Element in den Krätzen dar. Aus diesem Grund werden die Möglichkeiten der Behandlung von Hartzink und Oberflächenkrätze mit dem Ziel, das Eisen zu entfernen, untersucht.

Schlüsselwörter:

Tauchfeuerverzinkung – Rückstand – Krätze – Eisen – Rückgewinnung

## Traitement des déchets de zinc produits lors de la galvanisation à chaud

## Tratamiento de residuos de zinc proveniente de la galvanización en caliente por inmersión

### 1 Introduction

The hot-dip galvanizing process is one of the most commonly used processes of steel coatings to avoid corrosion of steel parts. As corrosion protection the metal zinc is used. Regarding to the kind of steel to be coated, there are several types of hot-dip galvanizing. Steel sheets are coated through continuous galvanizing, whereas steel parts and single components are coated in batch galvanizing process. The process of zinc galvanizing consists of several pre-treatment steps to ensure complete impurities removal followed by dipping particles in the molten zinc at a temperature of about 465 °C. In the pre-treatment steps that consist of cleaning, degreasing, pickling and fluxing, the liquid waste develops. In the molten zinc bath where the pre-treated steel particle is dipped in order to gain a zinc coating, several kinds of waste are produced. In continual galvanizing the bottom dross forms on the bottom of the zinc kettle due

to exceeding the maximum iron solubility in the molten zinc at the given temperature (at 465 °C the maximum iron solubility is 0.03 %). After exceeding the maximum iron solubility, iron starts to precipitate with zinc into the intermetallic phase  $FeZn_7$ . In this process aluminium in amount of 0.11 to 0.20 % is added. In that moment due to the higher affinity of iron to aluminium, iron starts to bond to the aluminium and creates an intermetallic phase  $Fe_2Al_5$  which has lower density than molten zinc and thus accumulates on the surface of the zinc bath. Such dross is called zinc top dross. In the dry batch galvanizing (without aluminium addition) bottom dross or so called hard zinc forms on the bottom of the kettle similarly as in the previous process. This bottom dross is basically an intermetallic compound  $FeZn_{13}$ . On the surface of the kettle zinc ash is also produced. In the batch process sal-ammoniac flux develops on the surface of the zinc bath due to the process characteristic. Hard zinc from the batch process and zinc top dross from the continuous



process are investigated in this study. In the present time, those kinds of wastes are sold to further processing. In the Slovak Republic over 2000 t of those wastes are generated every year. The price for hard zinc is multiplied by coefficient 0.7 to 0.4 and top dross 0.71 to 0.75 approximately according to current demand and purity [1-4].

## 2 Experimental

### 2.1 Material and methods

In the first step, the characterization of samples was conducted. Chemical composition was determined by AAS (Atomic absorption spectrometry), phase analysis by XRD (X-ray diffraction) using analyzer (X-ray diffractometer PANalytical X'pert PRO MPD).

The sample of hard zinc was further investigated by metallographic analysis. Microstructure was evaluated using light microscopy (LM). For LM analysis the microscope Olympus XC50 was used. The scanning microscope Tescan Mira 3 FE was used for SEM analysis.

In order to observe the behaviour of hard zinc during heating, its changes, either exothermic or endothermic, the DTA analysis (Differential Thermal Analysis) was conducted. For DTA analysis and evaluation Netzsch STA-449F3A-0861-M was used. The DTA curve provides data on the transformations that occur, such as glass transitions, crystallization, melting and sublimation. The area under a DTA peak is the enthalpy change and is not affected by the heat capacity of the sample [5].

In Figure 1, there can be seen the samples of hard zinc and zinc dross.



Fig. 1: Sample of hard zinc (left) and zinc dross (right)

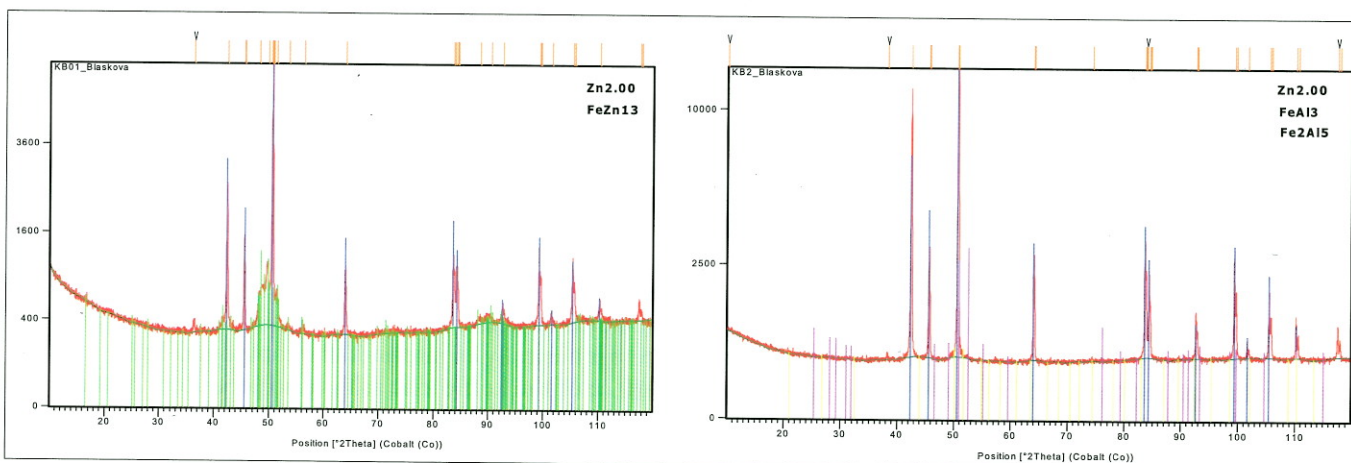


Fig. 2: The XRD pattern of the phase analysis: hard zinc (left) and zinc dross (right)

## 3 Results and discussion

From the conducted investigation of samples by AAS the chemical analysis is given in Table 1.

From Table 1 it can be seen that the hard zinc contains 2.55 to 2.81 % iron and the rest is zinc. Zinc top dross contains besides iron in range of 0.34 to 0.41 % also aluminium in amount of 0.6 to 0.69 % and the rest is zinc. The phase analysis of the samples can be seen in Figures 2 and 3 and Tables 2 and 3.

Table 1: Results of the chemical analysis

	Element	Chemical composition [%]		
Hard zinc	Fe	2.81	2.55	2.67
	Zn	rest	rest	rest
Zinc dross	Fe	0.37	0.41	0.34
	Al	0.60	0.64	0.69
	Zn	rest	rest	rest

Table 2: Result of the hard zinc phase analysis

Ref. Code	Name of compound	Chemical formula
96-900-8523	Zinc	Zn
03-065-1238	Iron zinc	FeZn <sub>13</sub>

Table 3: Result of the zinc top dross phase analysis

Ref. Code	Name of compound	Chemical formula
96-900-8523	Zinc	Zn
00-001-1265	Iron aluminium	FeAl <sub>3</sub>
00-001-1228	Aluminium iron	Fe <sub>2</sub> Al <sub>5</sub>



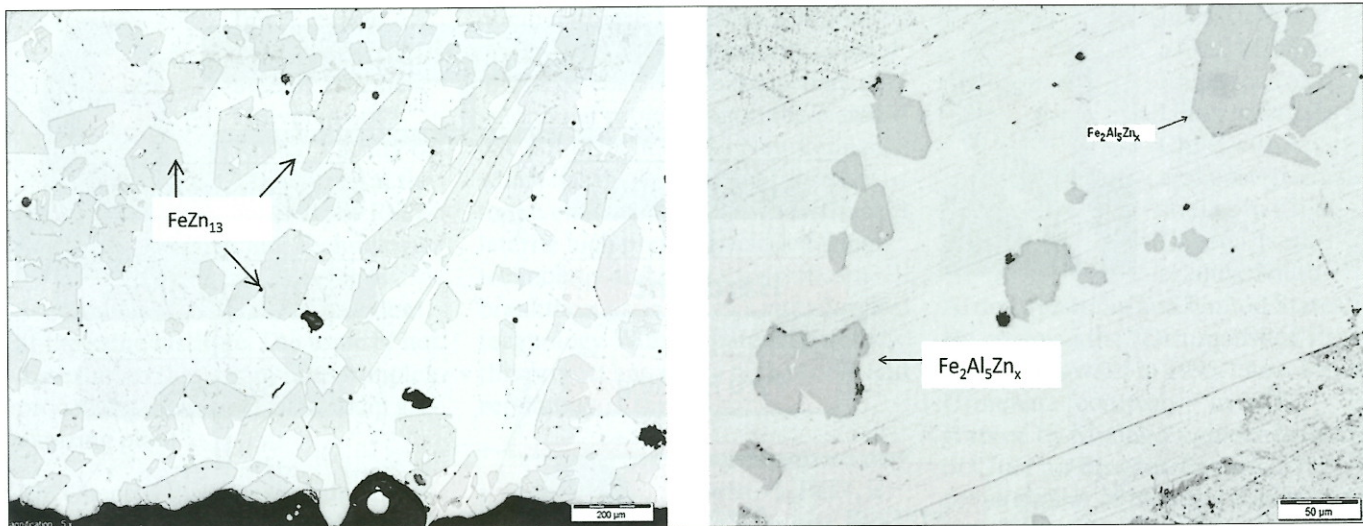


Fig. 3: Metallographic observation of hard zinc (magnification 5×) (left) and zinc dross (magnification 20×) (right)

The result of the phase analysis of hard zinc shows that iron is bonded to the zinc into the intermetallic compound  $FeZn_{13}$  phase and beside the phase there is metallic zinc presented as a matrix.

The result of the phase analysis of zinc dross shows that iron is bonded to the aluminium into the intermetallic compound  $Fe_2Al_5$ , and  $FeAl_3$ , respectively. Beside those phases there is metallic zinc present as a matrix.

The darker objects in Figure 3 represent intermetallic compounds whereas the lighter areas or surrounded area represent zinc matrix. According to the magnification it can be seen that the size of the  $FeZn_{13}$  phase varies in range of 50 to 200  $\mu m$ . The size of the  $Fe_2Al_5$  phase varies in range of 20 to 100  $\mu m$ .

In Figure 4, there can be seen the result of the DTA analysis of the hard zinc.

Under the temperature of approximately 420 °C the zinc starts melting as it is displayed by the endothermic peak. Reaching the temperature of 530 °C the intermetallic phase  $FeZn_{13}$  transforms into the intermetallic phase  $FeZn_{10}$  (pre-

sented as second smaller endothermic peak). At a temperature over 630 °C this phase dissolves completely in the molten zinc (the third endothermic peak). The evaluation of this DTA result was conducted in connection with the binary Fe-Zn diagram. The result of analysis showed residual mass in amount of 96.98 % at 748.1 °C. That means about 3 % of the sample vaporized at the temperature of 748.1 °C. This phenomenon can be explained by higher partial zinc pressure during analysing and thus zinc started slowly to vaporize. The partial zinc pressure can be calculated as follows:

From the HSC Chemistry the standard Gibbs free energy was calculated. Expectation that zinc as liquid passes to the gaseous form at the temperature 750 °C resulted in  $\Delta G^0 = 15,305 J$ . By the given formula (equation 1) the partial zinc pressure was set up as  $p_{Zn} = 16,757 Pa$ .

$$\Delta G^0 = R \cdot T \cdot \ln \frac{P_{Zn}}{P_0} \quad (1)$$

Based on a research about treatment possibilities, the experimental proceedings have been built and proposed treatment methods are displayed in the scheme in Figure 5.

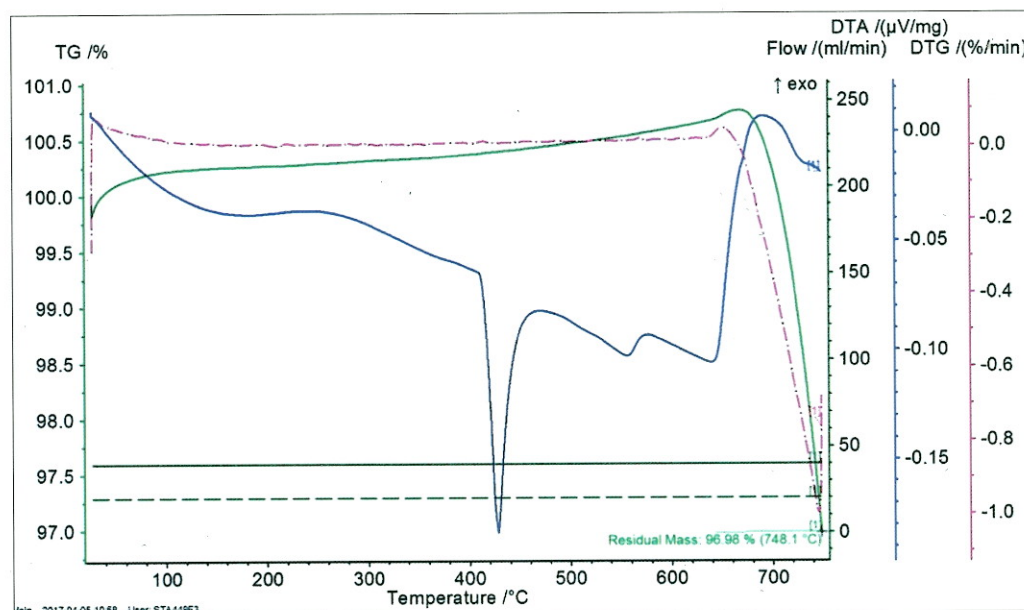


Fig. 4: Result of the DTA analysis of hard zinc



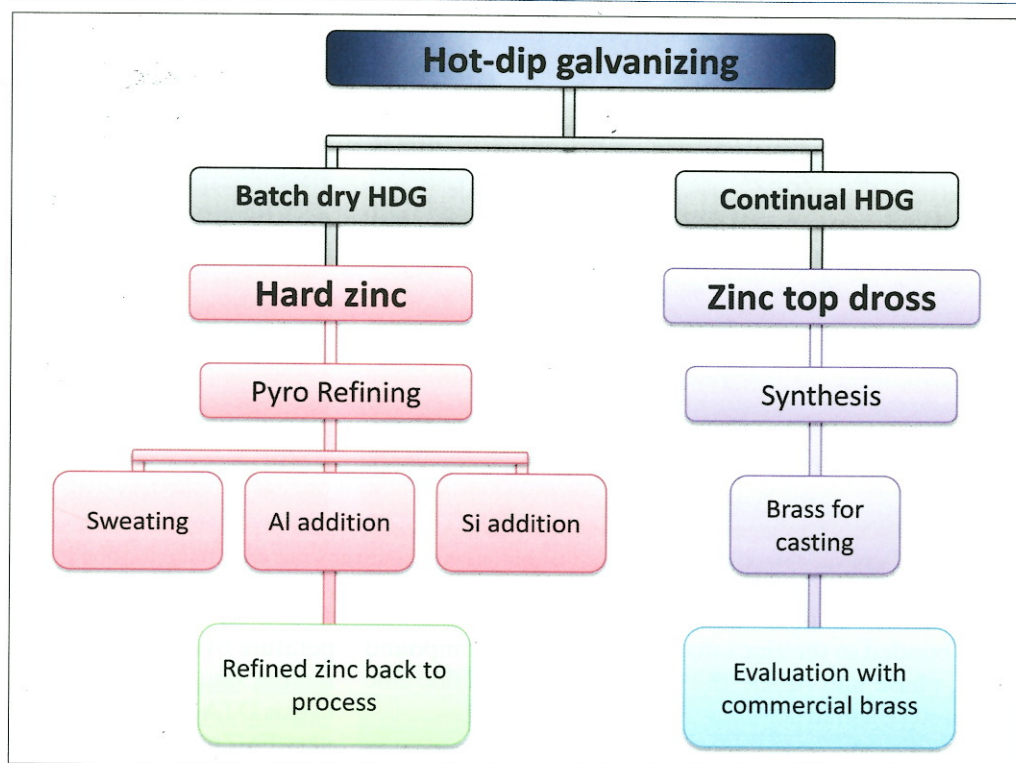


Fig. 5:  
Proposal of waste treatment

## 4 Conclusions

The present paper characterizes the chosen solid waste hard zinc and zinc top dross. The only impurity in those wastes is iron that is bonded into intermetallic compounds. The only possible way how to treat such kinds of waste is by pyrometallurgy due to its high zinc content. In the first stage the characterization of both kinds of waste were conducted by chemical analysis, phase analysis and the hard zinc was submitted also for DTA analysis. Proposed way of hard zinc treatment is by flame refining using sweating in a furnace with temperature gradient. Addition of chosen elements such as Si and Al will be investigated, too. The top dross will be used for synthesis of brass for casting and its characteristics will be investigated.

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